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INTERSTATE COUNCIL FOR STANDARDIZATION, METROLOGY AND CERTIFICATION
(ISC)

**33758—
2021**

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357/ 7 « 7 « »

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357/ 7 «

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26 2021 . 142-) (-

(31001004-97	no	(3108) 004—97	«
		BY KG RU TJ UZ UA	« »

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2021 . 1007- 33758—2021
1 2022 .

5 33758—2016

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34057.
632 633..... 43

33758—2016,

31446;

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34004;

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34057.

632—80

633—60.

34057. 632 633

Casing, tubing and couplings for them. Basic parameters and inspection of thread connections. General technical requirements

— 2022—03—01

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9376 (2632-1—85. 2632—85) ().

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31446 (IS011960:2014)

34004

34057

(www.easc.by)

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34004.

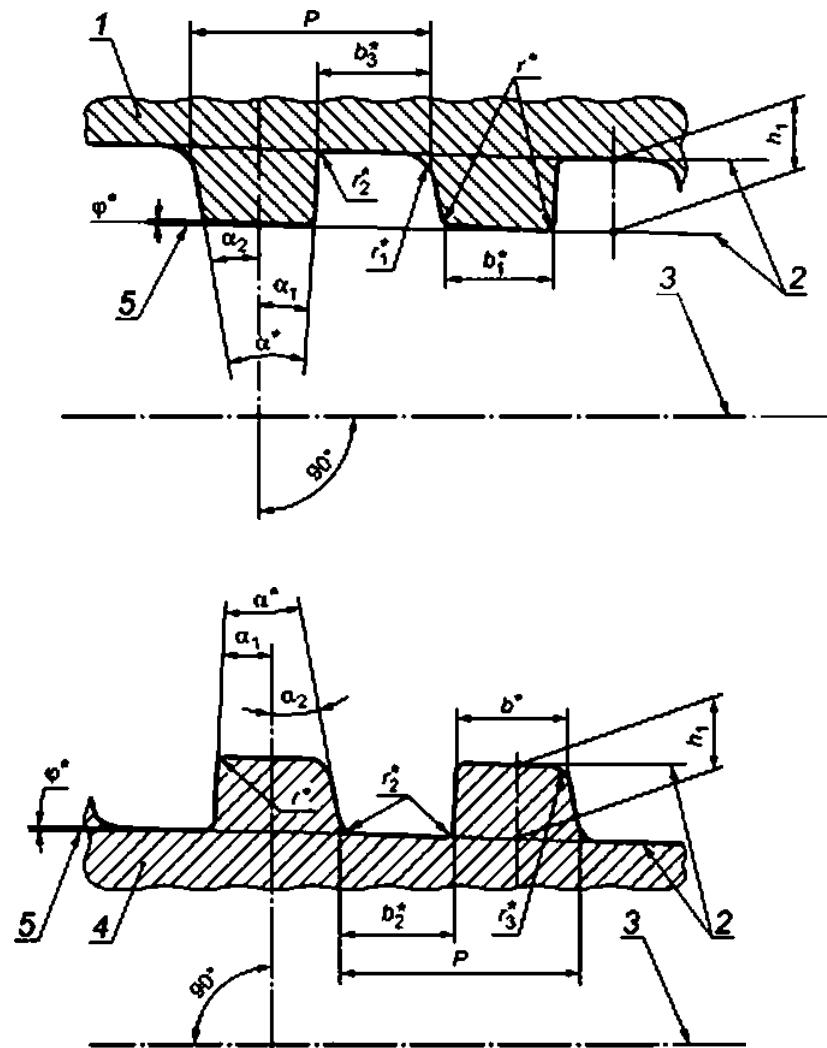
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	5.08	±0.05 25.4 "
,	1.60	±0.10 ±0.03

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«2	10*	±
* , *	2.29	—
${}^2 t {}^3$ *	2.43	+0.05
:		
*	0.20	+0.05
	0.80	-0.05
2*	0,20	-0.05
3*	0.80	+0.05
,	1°47'24"	—
25.4	1.59	2
,		
..		25.4
25.4	,	,

2—

25.4

				26.4
,		,		
193.66	.193.66	193.66	.	.193.68
+0.06	+0.06 -0.03	-0.06		+0.03 -0.06
+0.04	+0.05 -0,01	-0.04		+0,01 -0,05

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5.2.2

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3 4.

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 L_c

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5.2.4

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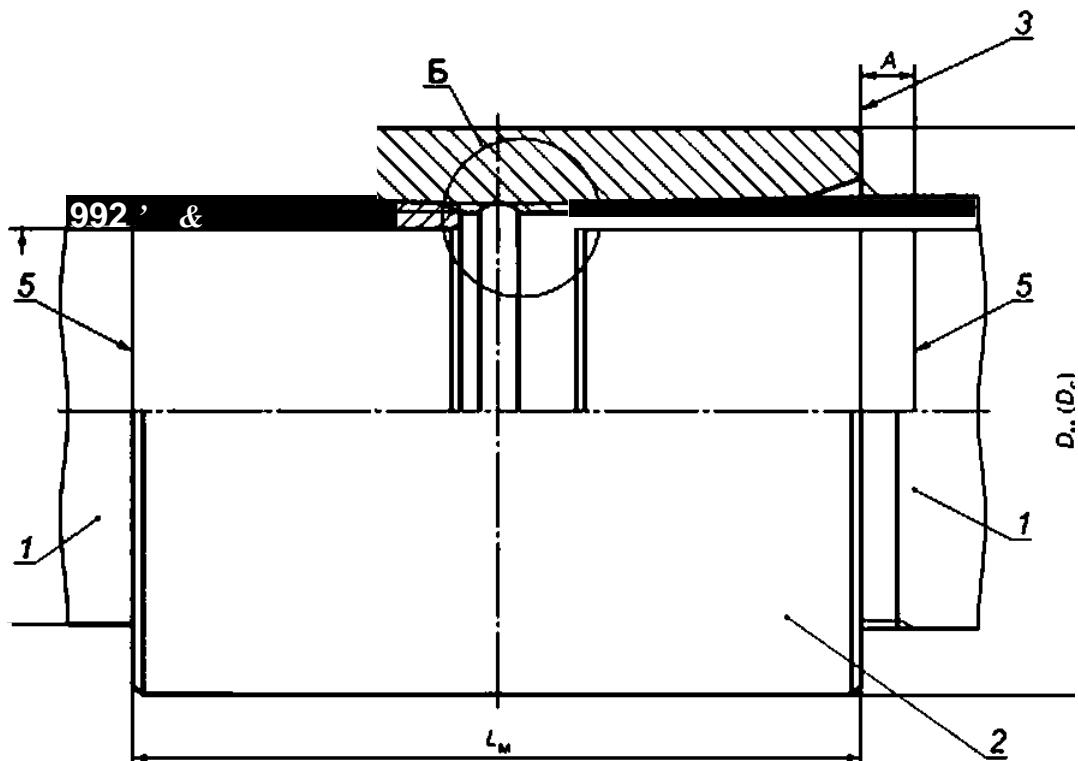
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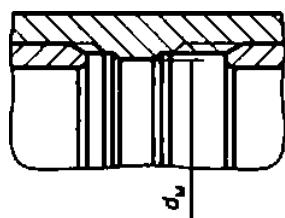
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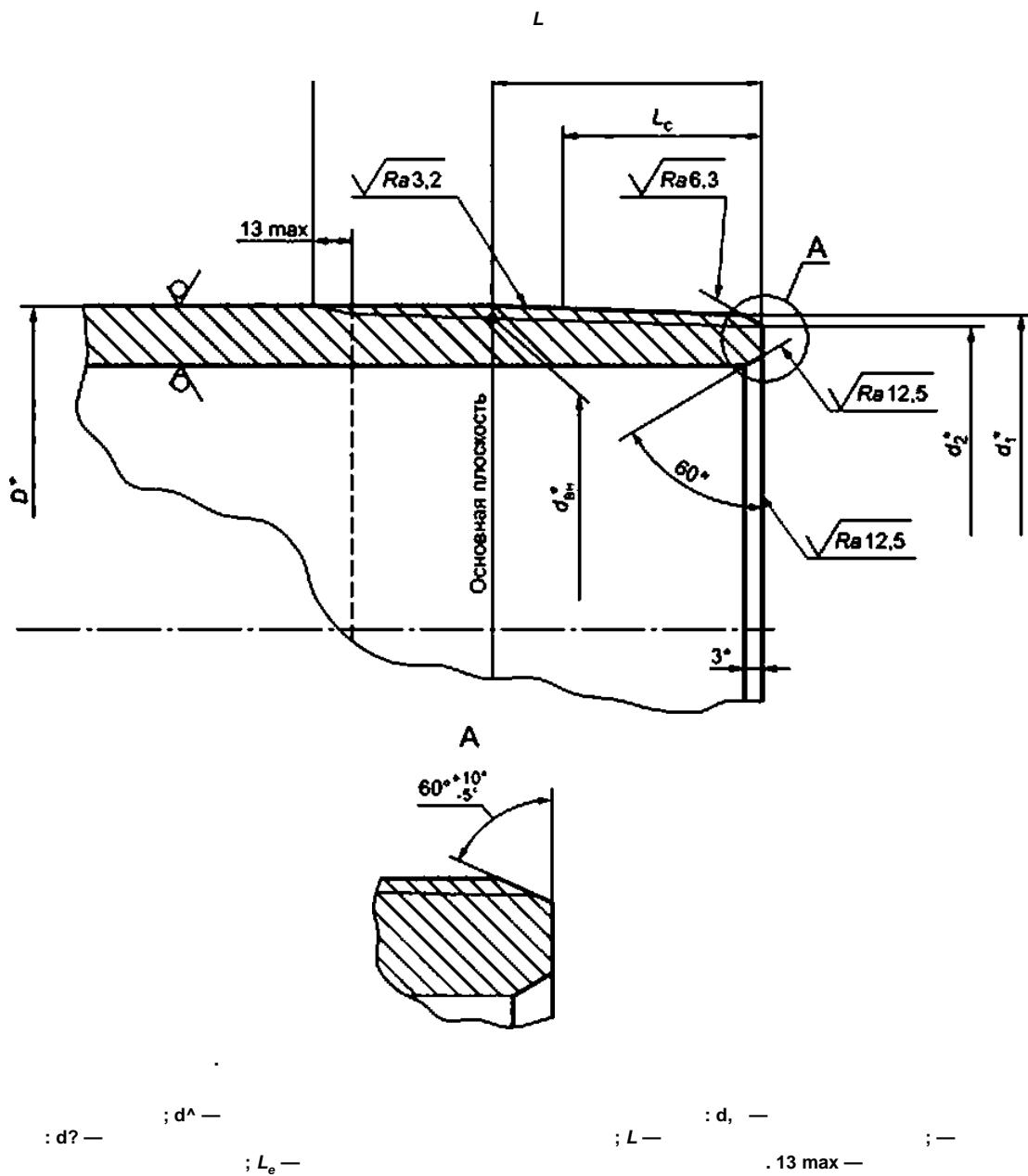


(101.60)

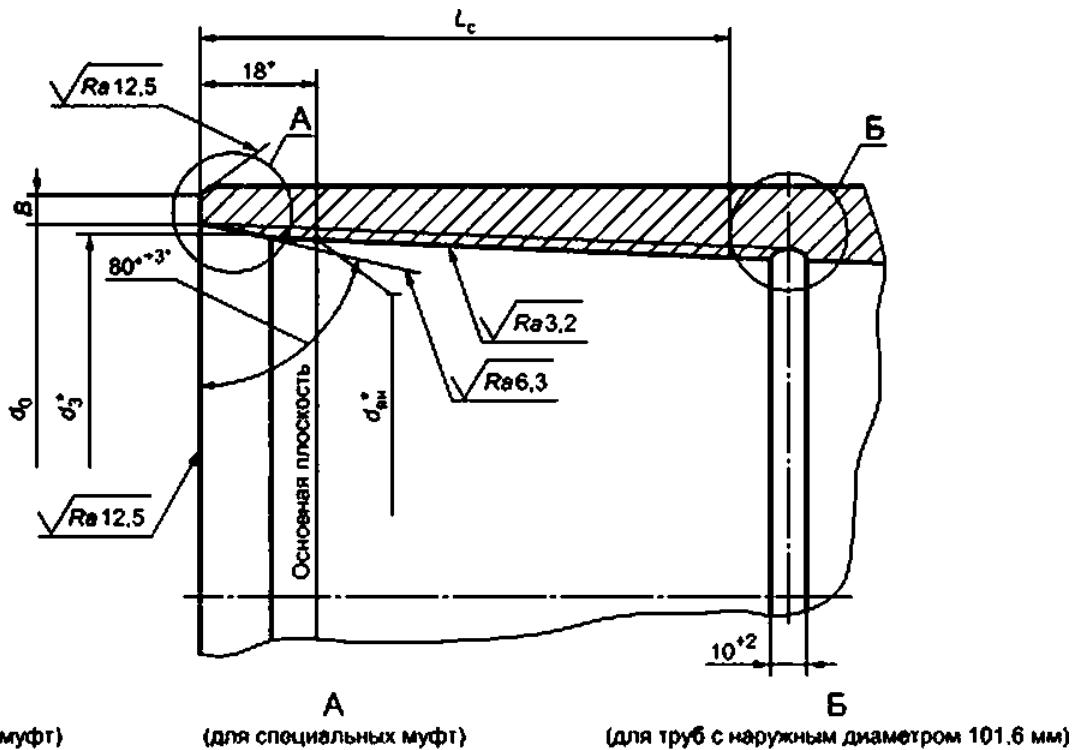
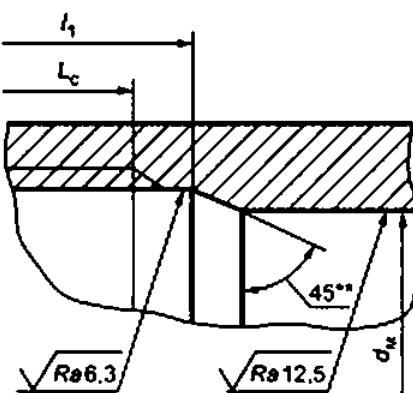
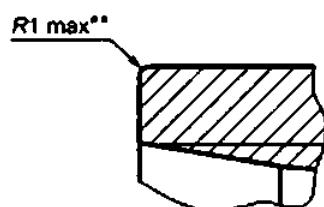
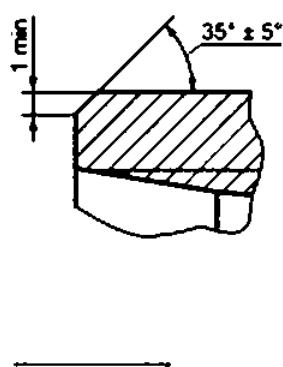


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 ; t— . L_M — ; —

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A
(для обычных муфт)A
(для специальных муфт)Б
(для труб с наружным диаметром 101.6 мм)

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 d_{ji} —
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101.60	101,60	98.400	99287	96.087	66	37	27	110	
114.30	114,30	111.100	111,675	108.475	74	42	32	14.0	
127.00	127,00	123.800	124,250	121.050	76	44	34	14,0	
139,70	139,70	136.500	136.700	133,500	80	48	38	14,0	
146,05	146.05	142.850	143.050	139850	80	48	38	14,0	
168,28	168.28	165.075	165.025	161825	84	52	42	14,0	
177.80	177.80	174.600	174.300	171.100	88	56	46	14.0	
193.68	193.68	190,475	189.925	186.725	92	60	50	14,0	
219.08	219.08	215,875	214.950	211.750	98	66	56	14,0	
244.48	244.48	241.275	240.350	237.150	98	66	56	14.0	
273.05	273.05	269.850	268.925	265.725	98	66	56	14.0	
298.45	298.45	295,250	294.325	291,125	98	66	56	14,0	
323.85	323.85	320,650	319.725	316525	98	66	56	14.0	
339.72	339.72	336525	335.600	332,400	98	66	56	14.0	
* i^o-10-									
— 4									

33758—2021

4 —

				*06	$t^o_{1.0}$	< ₃	*	> ₂₀	< ₅	L_c
101.60	114.00	110,0	190,0	98.400	90.0	103,8**	99.525	1.5	86	74
114.30	127.00	1238	170,0	111.100	—	116.5	112.225	3.0	—	78
127,00	141.30	1365	174.0	123800	—	129.2	124.925	4.0	—	78
139.70	153.70	1492	182,0	136500	—	141.9	137.625	3.5	—	82
146.05	166.00	156,0	182,0	142850	—	148.3	143,975	65	—	82
16828	187,70	177,8	190,0	165.075	—	1705	166200	6.0	—	86

D			obj ^A	10.5	d,,	1.0	“ dj	M [“] iee	2 ⁴⁵	L _c
177,80	194,50	1873	198,0	174.600	—	180.0	175.725	4.5	—	90
193.68	215.90	206,4	206,0	190.475	—	195.9	191.600	7.5	—	94
219.08	244.50	2313	218.0	215375	—	221.3	217.000	9.0	—	100
244.48	269.90	257,2	218.0	241275	—	246.7	242400	9.0	—	100
27305	298,50	285,8	218,0	269350	—	275,3	270.975	85	—	100
298.45	323.85	—	218.0	295250	—	300.7	296375	85	—	100
32335	350,52	—	218.0	320350	—	326.1	321.775	95	—	100
339.72	365,10	—	218.0	336325	—	342.0	337.650	85	—	100

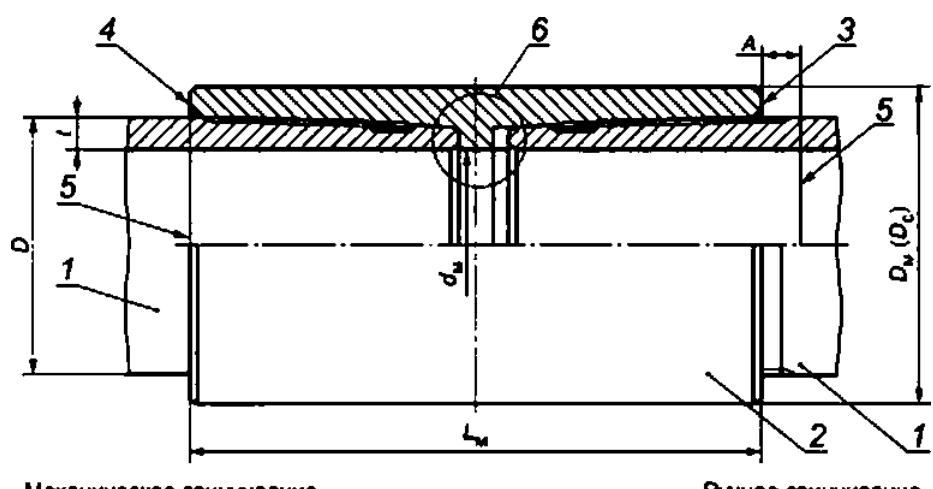
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±0.5

$$t_r = 0.875 - 0.5(1.0 - d_2). \quad (1)$$

t_r	—	0.1	;
f	—		
D	—		
d_2	—		
5.2.5		1.00	
5.2.6			
- 0.75	—		
• 3.00	—		
5.2.7	1	(2)	
		5.0	
5.3			
5.3.1		5.	



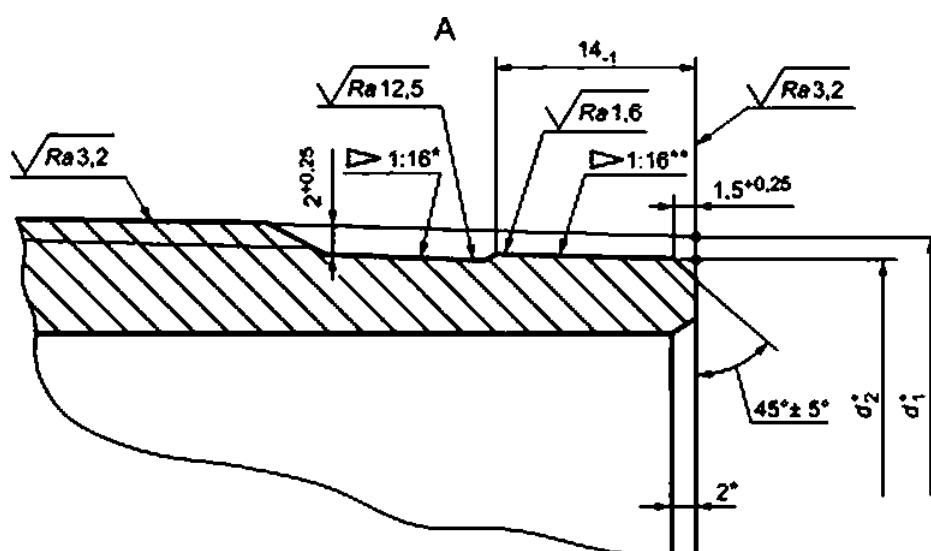
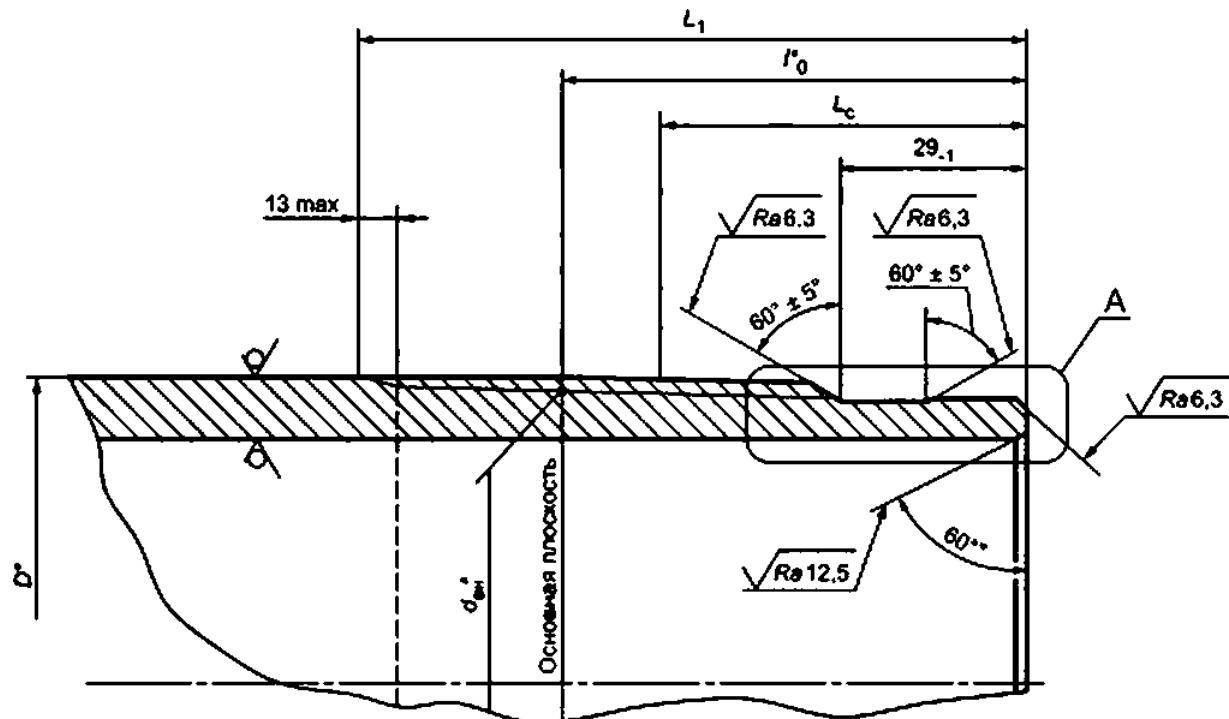
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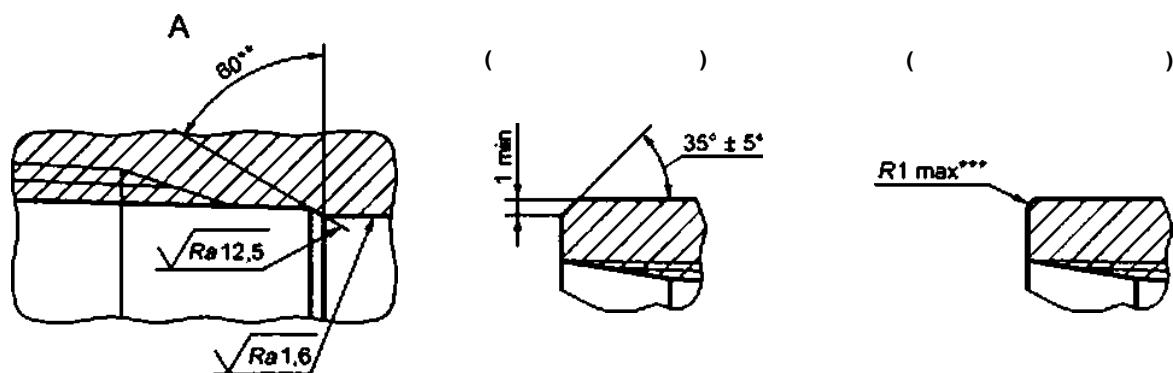
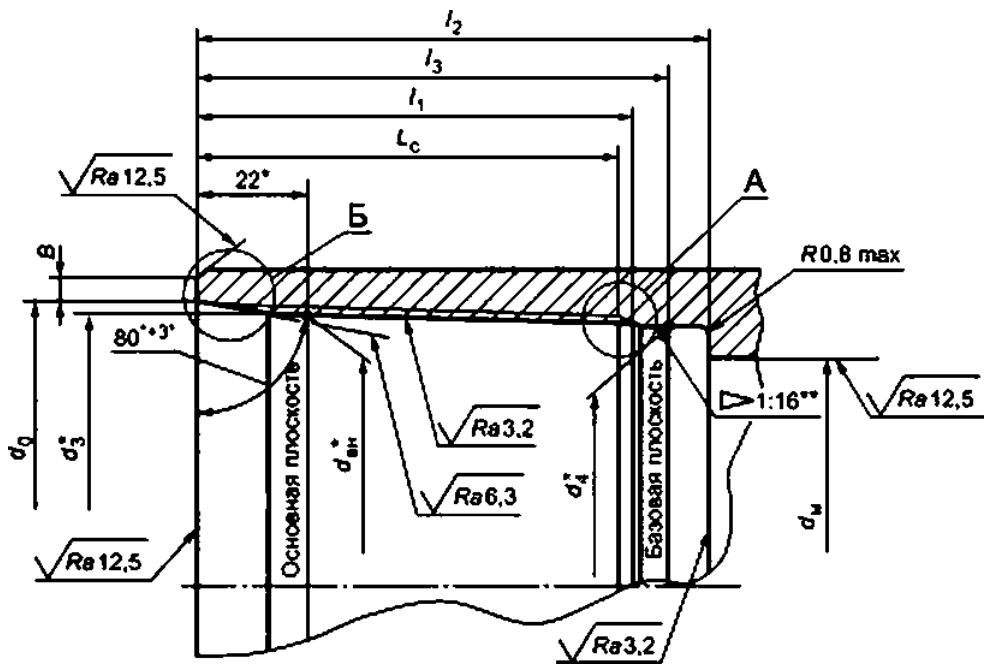
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5.3.2

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 ± 0.03 $; d_e —$ $; L_e —$ $.13 \text{ max} -$



d_0 — ; d_1 — ; d_M — ; d_4 — ; t_c — ; 60° :
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*	D	4^			L., -1.0			L_c*
114.30	114.30	111.100	110.175	106.375	98	66	56	10,0
127,00	127,00	123.800	122,750	118.950	100	68	58	10,0
139,70	139,70	136.500	135,200	131.400	104	72	62	10,0
146,05	146.05	142.850	141.550	137.750	104	72	62	10,0
16828	168.28	165,075	163.525	159,725	108	76	66	10,0
17780	177,80	174,600	172.800	169,000	112	80	70	10,0
193,68	193.68	190.475	188.425	184.625	116	84	74	10,0
219,08	219.08	215,875	213.450	209.650	122	90	80	10,0
244,48	244.48	241,275	238 850	235.050	122	90	80	10,0
250,83	250.83	241.275	238850	235.050	122	90	80	10,0
273.05	273.05	269.850	267 25	263.625	122	90	80	.
323.85	323.85	320.650	318225	314.425	122	90	80	10,0

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										9.19						
										10.70						
										11,10						
127,00	141,30	136.	210.0	123,800	129,2	125,175	119.000				110,0	98	90	84	74	4.0

D			4 - 1.0	cq	t	<T _w 0.5 -1.0	V 10	-	V -10	1	8*		
	*>	4 - *											
139.70	153.70	149,20	218,0	136.500	141,9	137,875	131450	9.17	122.0	102	94		
								1054	119.0				
146.05	166.00	156.00	218.0	142.850	148,3	144225	137800	8.50	132.0	102	94		
								9.50	130.0				
								10.70	126.0				
168.28	187,70	177,80	225.0	165.075	170,5	166450	159,775	8.94	151.0	106	98		
								1059	148.0				
								12.06					
177.80	194.50	187,30	234.0	174.600	180,0	175.975	169,050	9.19	160.0	110	102		
								1026	158.0				
								11.51					
								12,65					
								13.72					
								15.00					
193.68	215.90	206.40	242.0	190475	195.9	191850	184.675	9.52	175.0	114	106		
								10.92					
								12,70	172.0				
								1427					
								15.11					
								15.88					
219.08	244.50	231.80	254.0	215875	221.3	217250	209.700	8.94	203.0	120	112		
								10.16					
								11.43	198,0				
								12.70					
								14,15					

<i>D</i>				^A	4	<%. 1.0	-	-	1	d,, 0,5 -1,0	10	*	or	V -1	-	-					
244,48	269.90	257,20	254,0	241,275	246,7	242.650	235,100		8,94	226.0	120	112	106	96	9.0						
									10,03	223.0											
									11,05												
									11,99												
									1384												
									1590												
250,83	269.90	—	254.0	241.275	246,7	242.650	235.100	1588	223.0	120	112	106	96	9.0							
273,05	298.50	285.80	254.0	269.850	275,3	271.225	263.675		8,89	256.0	120	112	106	96	8.5						
									10,16												
									11,43												
									1257												
									1384												
									15,11												
323,85	351,00	—	254.0	320.650	326,1	322.025	314.475		1650	306.0	120	112	106	96	8.5						
									9,50												
									11,00	303.0											
									12,40												
									14,00												

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5.3.3

 L_c

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193.68

*

219,08

5.3.4

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146,05

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16828; 219,08; 244.48; 273.05

8.00:8.89; 8,94

323.85

9.50

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2.5

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3.0

(2)

3.0

-

(2)

2.5

3,0

$$= 0.875 - 0.5 (1.0 - d_2). \quad (2)$$

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D —

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d₂ —

5.3.5

1.00

5.3.6

• 0.75 — ;

• 3,00 — 1

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5.3.7

(5)

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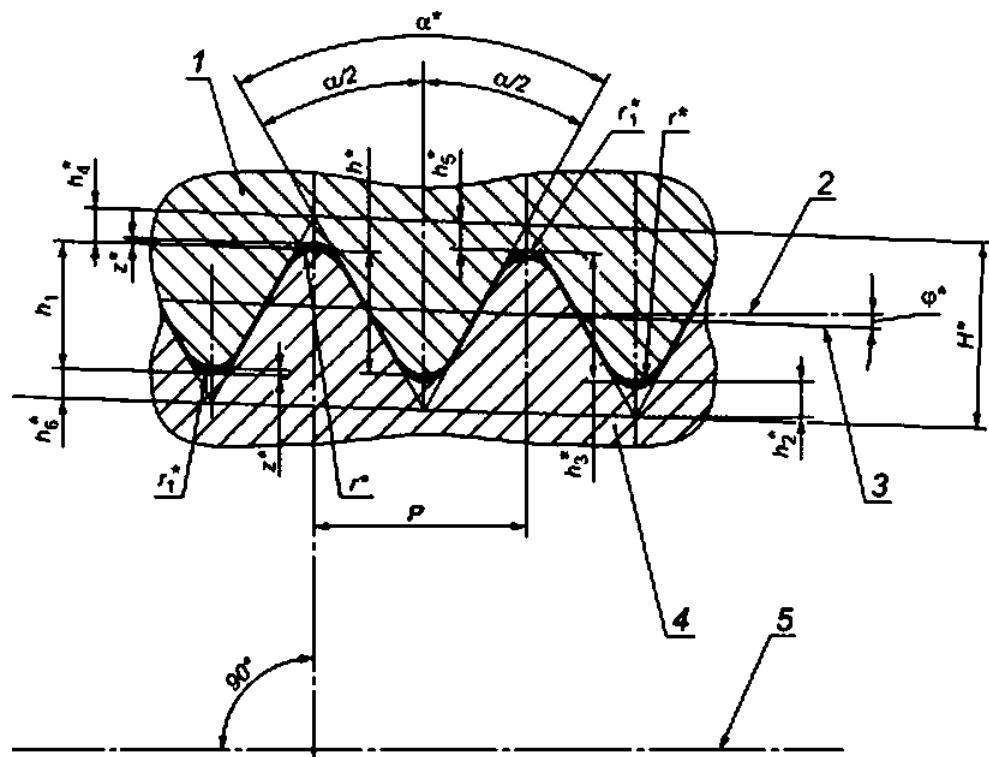
6.1

6.1.1

8

8

7.



1 — ; \$ — ; 2 — , , /2 — . 3 — ; 4 —
 — ; ftg. h_g — ; h — ; — ; q — ; — ; —

— 1:16 0.0625 /

8 —

7 —

25.4				
	10		8	
	2.540	± 0.075 25.4 **; ± 0.120	-	3,175 ± 0.075 25.4 °; ± 0.120
*	2.200	—	2.750	—
h'	1.336	—	1,734	—
$ftp \ ft_3$	1.412	$+0.050$ -0.100	1,810	$+0.050$ -0.100

25.4					
10					
*	60'	—	60'	—	
«/2	*	±	30'	*1'	
	0.432	+0.045	0.508	+0,045	
	0.356	-0.045	0,432	-0,045	
?*. *	0.432	—	0.508	—	
*. fig •	0.356	—	0,432	—	
z*	0.076	—	0,076	—	
< *	V4T24'	—	1'47'24*	—	
25.4		1,59	+0.09	1,59	+0,09
			-0.06		-0,06
			+0.06		+0,06
			-0,09		-0,09

,

**

25.4

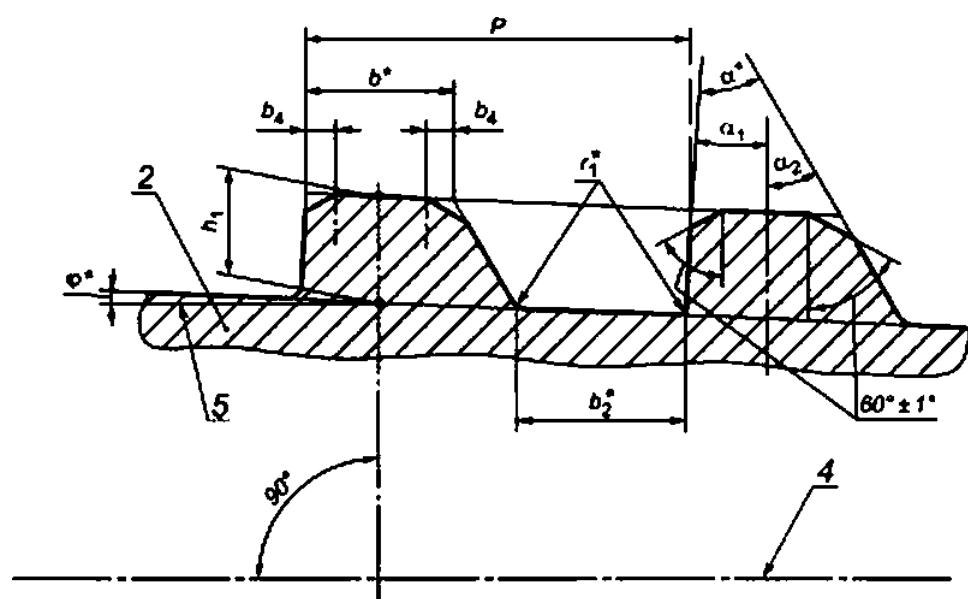
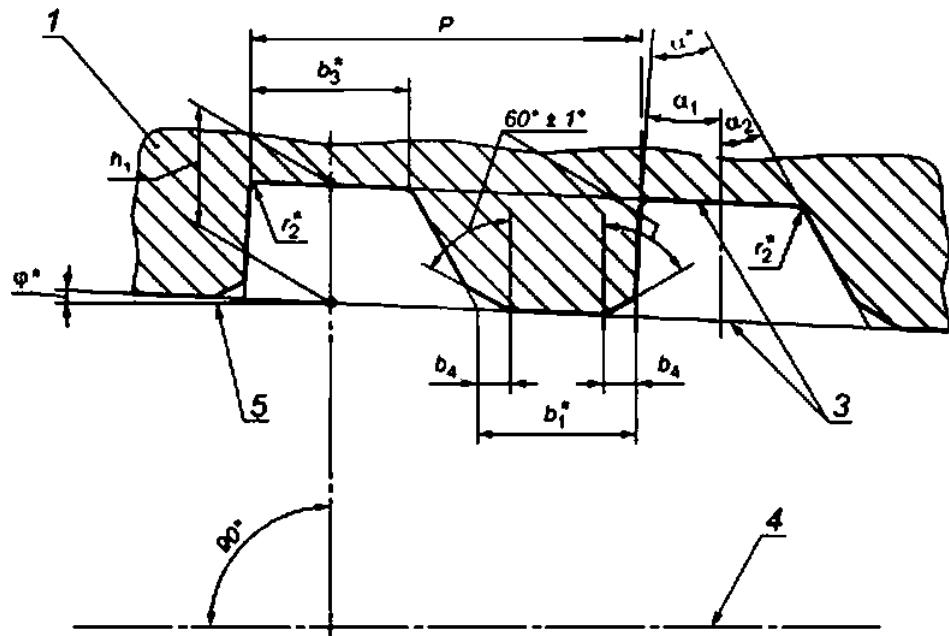
25.4

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6.1.2

-		60.32	101.6	-
9	8.	114.3	—	10
8.				



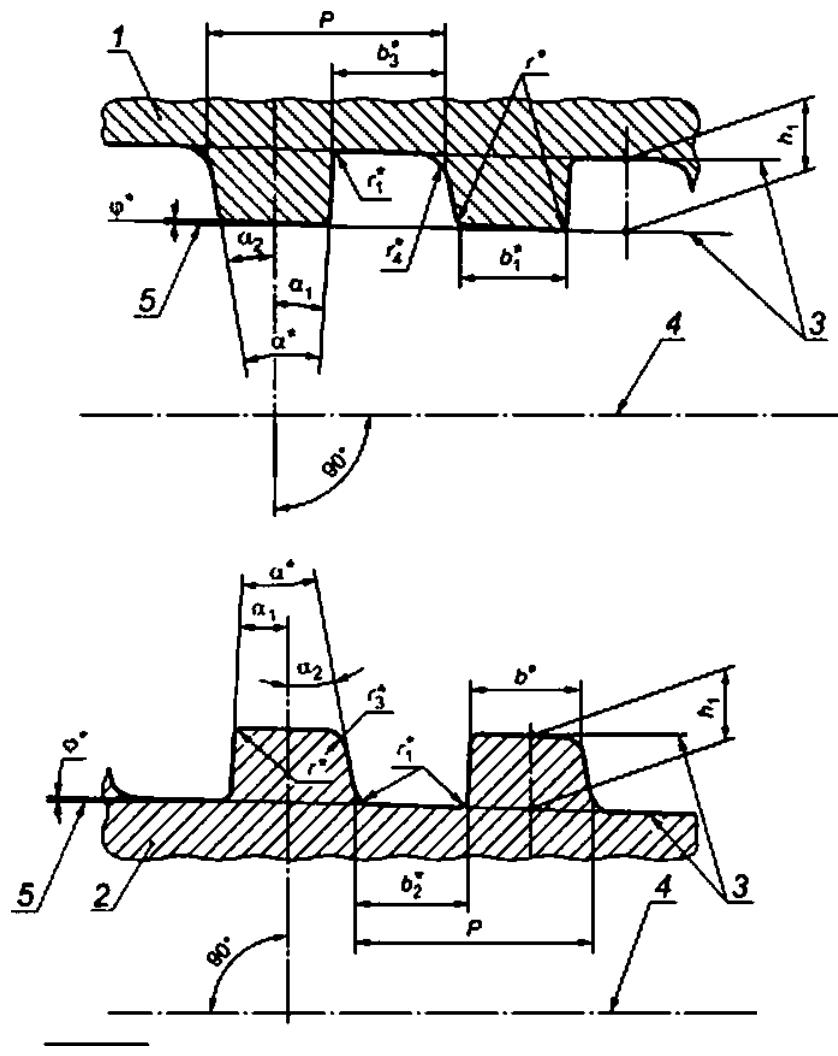
— .2— ; 3~ ; 4— ; 5— ,
 , b_j . : — ; (2— ; .— ; : — ;
 q. 2— : 4— ; : 1— ; < - ; : — ;

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4,233 — 1:12 0,0833 / .

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9—

60,32 101,60



1 — ; 2 — ; 2 — ; 2 — ; 4 — ; 5 —
 : — : — : o . . ~ — : 6. 6, — ; — ; —
 ; q. q —

1
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 5.080 — 1:16 0.0625 / .

10 —

114.30

8 —

	80.32	101.80	.	114,30
	4,233	±0.040 25.4 **; ±0.080	5.080	±0.050 25.4 *; ±0.100
"	1.20	+0.05	1.60	±0.03
	1.30	+0.05	1.60	±0.03
,	33*	—	13*	—
,	3'	±	3'	±
2	30'	±1"	10	±1'
,	0.20	-0.05	0,20	+0,05
'	0.05	-0.05	0.20	-0.05
,	0.80		0.80	+0.05
,	0.80		0.80	-0.05
,	1.659		2.29	
?	1.600		2.29	
V	1.800	+0.05	2.43	+0.05
,	1.794	+0.05	2.43	+0.05
b_t	0.30	+0,05	—	—
< *	2°23'09"	—	1°47'24"	—
25.4		+0.04'* 2.12	1.59	+0.04
				-0.04

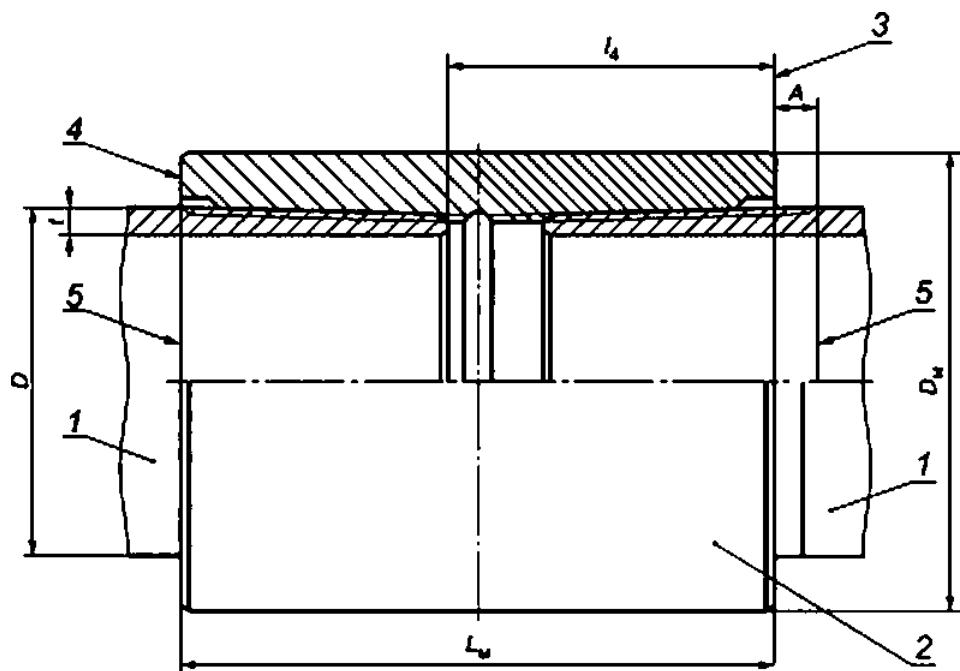
25.4

25.4

6.2

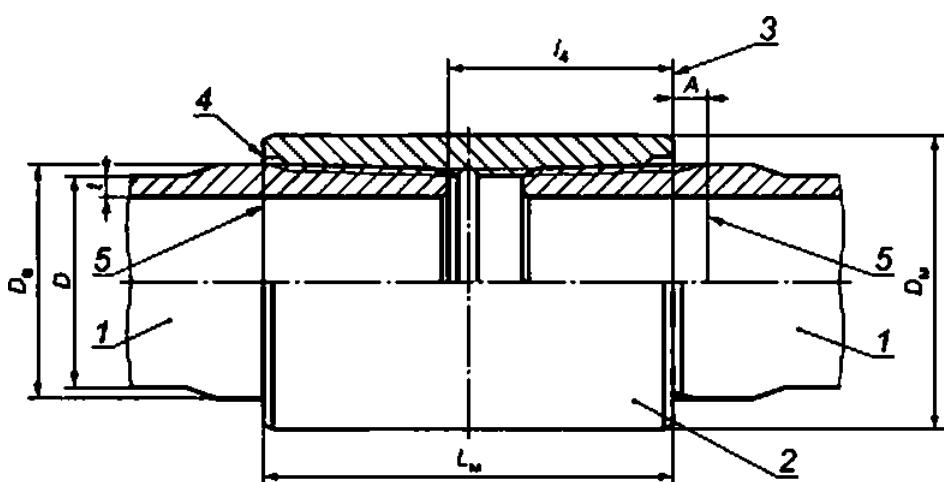
6.2.1

11 12.



1— ; 2— ; 3—
 ; — ; 5—
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11—



J— . 2— . 3—
 ; — . 5~
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12—

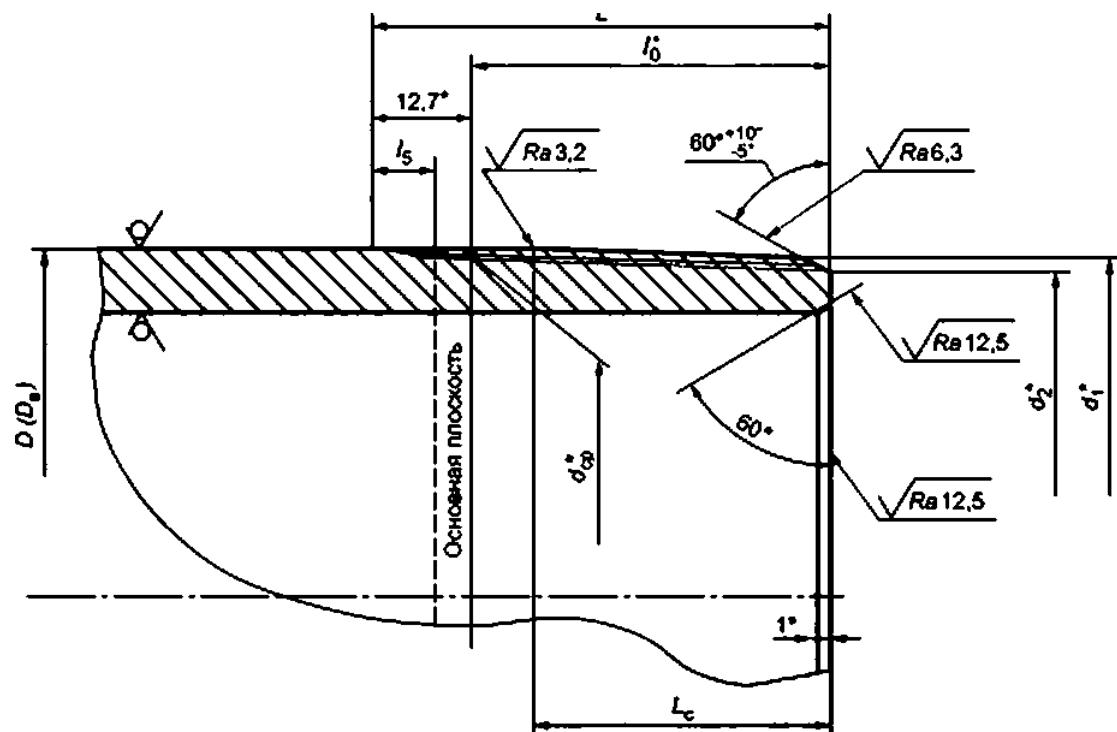
6.2.2

13 14

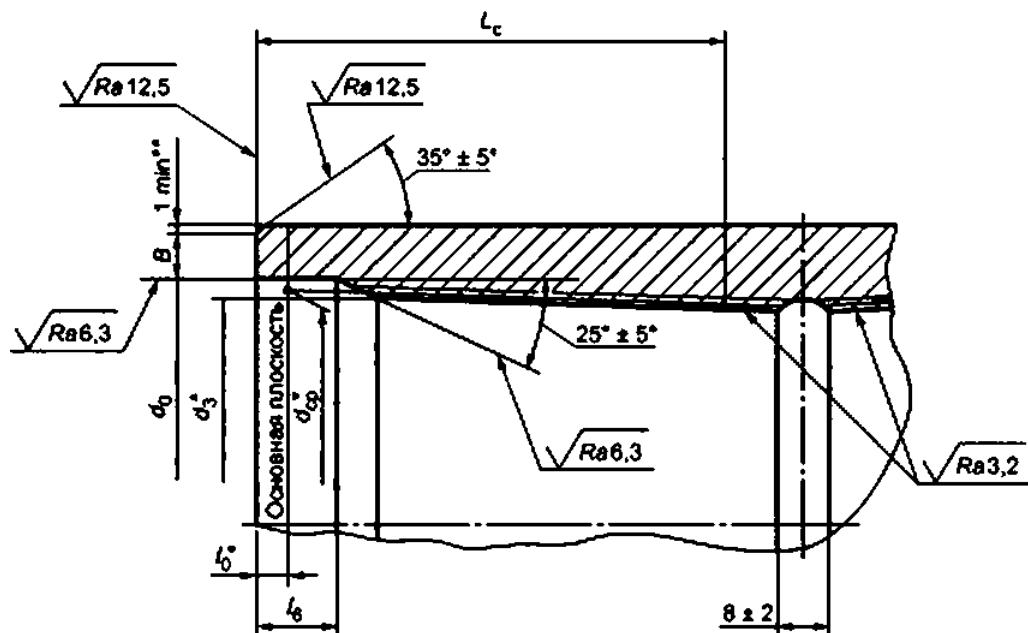
11 12.

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9 10,

 $D -$ $; D, -$ $\{ ; d_2 \sim) . d \wedge -$ $; L \sim , d, -$ $; -$ $-$ $;$ $L_o -'$

13 —



1g —

; L_c —; $J|Q \sim$

(13 -)

2

3

0.50

20*.

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9—

»	D		4		^	1					1 *
						*2	-				
33,40	3340	2540	32,065	32,382	29.568	29.0	±2.5	16,3	8	8.8	
42.16	42,16		40,828	40,948	38.124	32.0		19,3		115	
48.26	4826		46,924	46,866	44.042	35.0		22.3		14.8	
60.32	60,32		58.989	58,494	55.670	42.0		29.3		21.8	
73.02	73,02		71.689	70,506	67.682	53.0		40,3		32.8	
88.90	88,90		87.564	85,944	83.120	60.0		47.3		39.8	
101,60	101.60	3,175	99.866	98,519	94.899	62.0	±32	49.3	10	39.3	
114,30	114,30		112.566	111,031	107.411	65,0		52,3		42.3	

• = $I_0 - 75$ 2540 . $L_c =$ 10,0

3,175 .

D			4®	4,	4?	1				1\$.	-
						-	-				
26.67	26,67	33.40	2,540	32,065	32283	29.568	29,0	±2.5	16.3	8	8.8
33.40	33.40	37.30		35.970	36,100	33,276	32,0		19,3		11.8
42.16	42.16	46,00		44.701	44,634	41,819	35,0		22,3		14.8
48.26	48.26	53.20		51.845	51662	48,833	37.0		24.3		16.8
60.32	60,32	65.90	3,175	64.148	63,551	59,931	50,0	±3.2	37.3	10	27.3
73.02	73.02	78.60		76.848	76,001	72,381	54.0		41.3		31,3
88.90	88.90	95.20		93.516	92294	88,674	60.0		47.3		37,3
101.60	10160	108.00		106216	104,744	101,124	64.0		51.3		41.3
114.30	114.30	120.60		118.916	117.256	113,636	67,0		54.3		44.3
* =/-75 2540 . $L_r = -10.0$ 3,175 .											

g

11 —

	-				8 »<				0 1	* 1.6 -05			
	£>				*9	*3							
33.40	48.30	84,0	2,540	32,065	312	35.0	29.0	8.0	7.7	2.0	5.0		
42,16	52.20	90,0		40828	39,973	43,8	32,0			2.5			
48.26	55,90	96,0		46,924	46,069	49.9	35,0			1.5			
60.32	73.00	110,0		56,989	58,134	61.9	42,0			4.0			
73.02	88,90	132,0		71.689	70834	74.6	53,0			5.5			
88.90	108,00	146,0		87564	86.709	90,5	60,0			6.5			
101.60	120,60	150,0	3,175	99866	96519	103.2	62,0	9.5	62	6.5	6.5		
114.30	132,10	156,0		112,566	111219	115,9	65,0			6.0			

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12 —

	-				<	dj	*08			%.*15 -05			
		L*											
26,67	42,20	64,0	2,540	32.065	31,210	35.0	29,0	6.0	7.7	2.0	5.0		
33.40	48.30	90,0		35.970	35.115	36.9	32.0			3.0			
42.16	55,90	96,0		44.701	43,846	47.6	350			25			
48.26	63,50	100,0		51.645	50.990	54.6	37			25			
60.32	77.80	126,0	3,175	64.148	62.801	67.5	50,0	9.5	62	35	6.5		
73.02	93,20	134,0		76.848	75.501	80.2	54.0			45			
88.90	114.	146,0		93.516	92.169	96.9	60,0			65			
101.60	127,00	154,0		106.216	104.869	109.6	64,0			65			
114.30	141.30	160.0		118,916	117569	122,3	67.0			75			

6.2.3

* 1.0		48,26		:	
(3).	1.0 ;		,		t_r
- 2.0			,		t_r
(3).	2,0 ;				
*				(3).	1.0 2.0
.					-

$$= 0,875f - 0,5 ((D + AD) - d_2). \quad (3)$$

, —		,	.	0.1 ;	
t —	,	;			
D —	,	;			
—			,	,	0.8
			101,60		
				0.9	
114,30 ;					

 d_2 —

6.2.4

:					
* 0,75 —		;			
- 3,00 —	1	.			
			1		1.00
				2.00	.

6.2.5

:					
* 0,100 —		26,67	60,32	;	
* 0,130 —		73,02	89,90	;	
- 0,150 —		101,60	114,30	.	

6.2.6

I_4 (11,12)		,			
(4)					
$I_4 = (\mathcal{E} - L) \pm 2$.			(4)

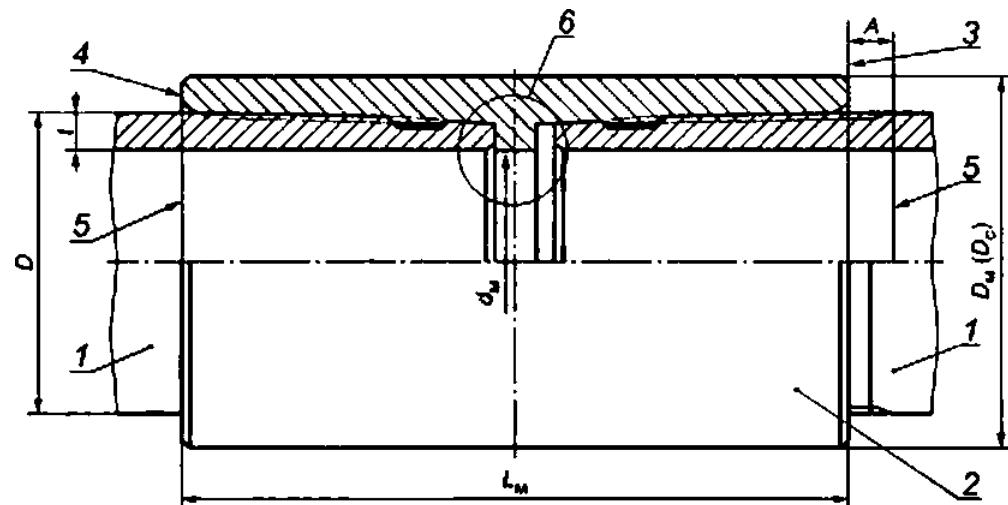
\mathcal{E} —	,	;			
L —	,	;			
—	,	.			

6.3

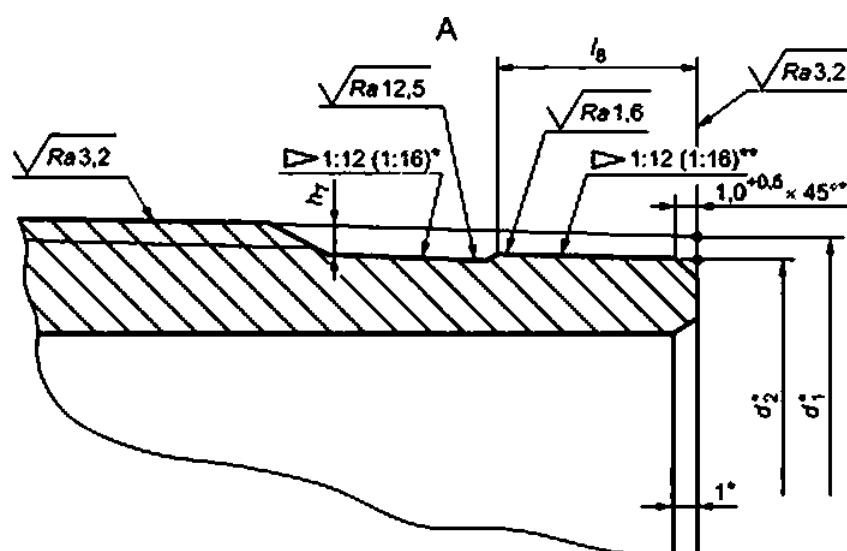
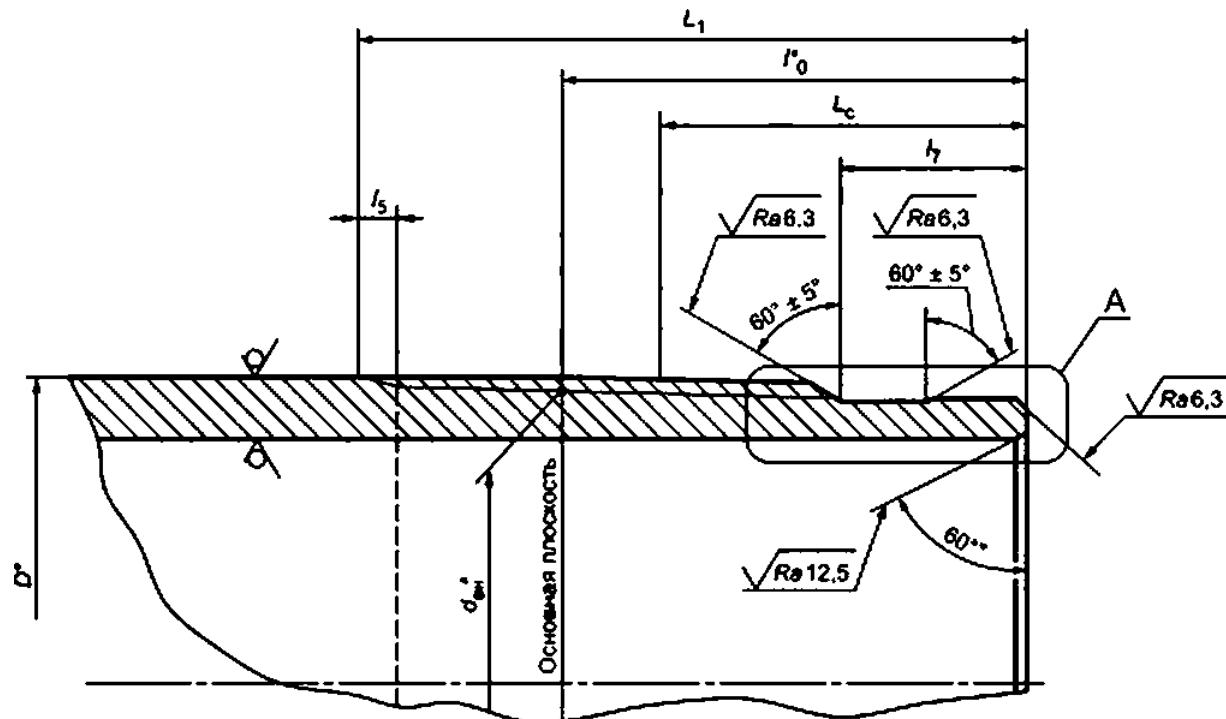
6.3.1 15.

6.3.2

16 17 14 15.



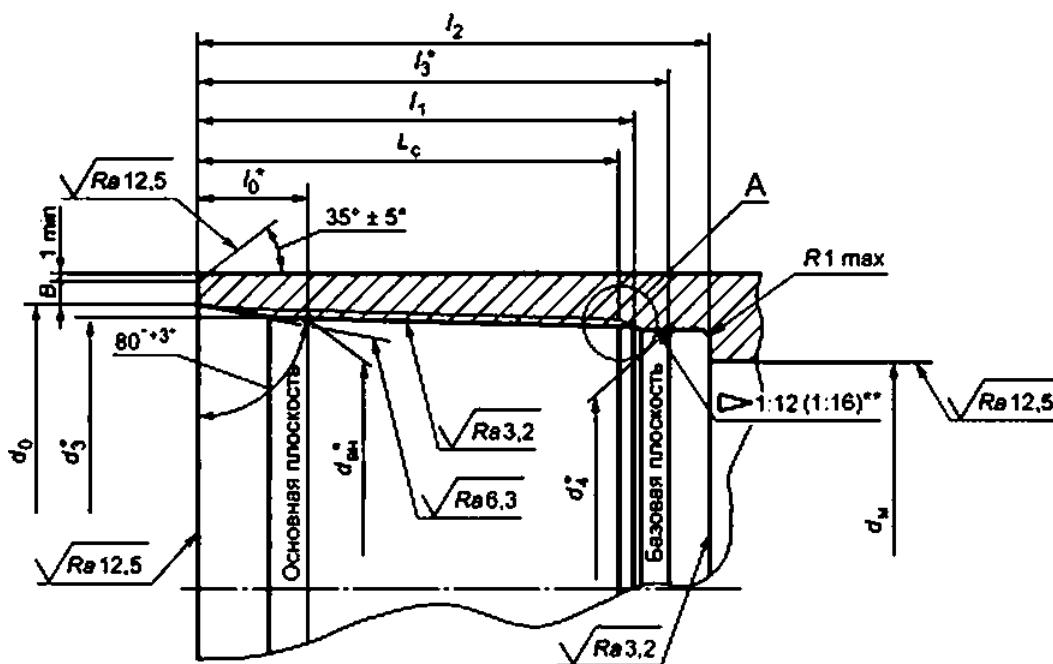
J — .2 — .3 ~
 .5 — ; — ; 4 —
 . $\varepsilon>$ — ; — ; ; ;
 . — ; I — ; ;
 — ; D_e — ; L_M —

 ± 0.03

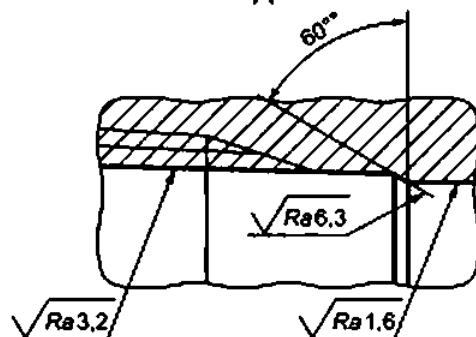
$: d, —$	$: d_2, —$
$: ft, —$	$: —$
$: L_e, —$	$: —$
$1:12 \quad 0.0833 \quad /$	60.32
$1:16 \quad 0.0625 \quad **$	114.30

101.60

16 —



A



10,06

d_3 —	d^* —	d_0 —	d_M —
; d_3 —	; d^* —	; d_0 —	; d_M —
60° ;	60° ;	(δ) —	J , ~
;	;	;	;
—	—	—	—
60.32	101.60	1:12 1:16	0.0833 0.0625 / —
114.30	—	—	—

17 —

14 —

«94	D		d _t	d _j	-1			-1.0	-1.0	«0.25	
60.32	6022	4.233	57,925	56575	54,175	65	45,0	10	20	1.60	36.5
73.02	73,02		70.625	69275	66,675	65	45.0				36.5
66,90	68,90		86500	84,317	81,917	75	55.0				46.5
101.60	101,60		99200	97.017	94,617	75	55.0				46.5
114.30	114.30	5.080	111.100	110.175	106.375	98	66,0	13	29	14	2.00
* Lc / ₀ -10,0		5.080 -8.5		4.233							56,0

* Lc /₀ -10,0

5.080 -8.5

4.233

15 —

D			d _t	d _j	4	10.5	1.0	7	1		
60,32	73.00	135,0	4.233	57.925	59.225	54.475	62.500	424	50,0	63,0	57
73.02	86.90	135,0		70.625	71.875	67,125	75.000	483	50,0		53
8820	108.00	155.0		86.500	87.700	82.117	91.000	5,00	50,0		43
101.60	120.60	155.0		99.200	100.350	94.767	104.000	551	62.0		155
114.30	132.10	205.0	5.080	111.100	112.600	106.425	116500	7,01	60.0		3.5
								6.45	74.0		4.4
								724	74.0		
								8.00	72.5		
								952	70.0		
								650	68.0		
								6.65	68.0		
								658	100.0		
								7.00	100.0		

6.3.3

- 1.2	60.32	,	t_r	(5)
1.2 :				
- 1,5	73.02		5.51	
(5)	1.5 ;			t_e
• 1,8			(5)	1.8 ;
-			(5),	1.2 . 1.5
1.8	.	.		

$$f_r = 0.875f - 0.5((D+AD)-d_2). \quad (5)$$

t_r —				
,	.	0.1 ;		
f —	,	;		
D —	,	:		
—			,	0.8
		101.60	0.9	
		114,30 ;		
d —	d_2 —		,	
6.3.4				
• 0.75 —		;		
• 3,00 —	1			
6.3.5			:	
- 0,100 —		60.32 ;		
• 0.130 —		73.02 89.90 ;		
- 0.150 —		101,60		
6.3.6			(.)	15)

7

7.1

7.1.1

7.1.2

7.1.3

7.1.4

7.2

7.2.1

7.2.2

• 25.4 —

- 12.7 —

25.4

25.4

• 12.7 —

- 25.4 —

25.4

25.4

16.

16 —

	3.175	1.83	
	2.540	1.45	±0.05

(50°)

3°.

17.

17 —

	4,233	1,44	
	5,080	2.29	
	4,233	1,44	
	5,080	1.57	±0.05

(50°)

2.29

7.2.3

25575

25576.

7.2.4

7.2.5

7.3

7.3.1

25575. 25576. 10654.

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250

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1

7.3.2

, (6). 0,01

= 0,0030.

(6)

D—

7.4

7.4.1

10654 25576.

- 1.6	—	26.7	60.3	;
- 2.1	—	73.02	88.9	;
- 2.4	—	101.6	114.3	.
- 1,2	—	60,3	;	
- 1,6	—	73,02	88,9	;
- 1,8	—	101,6		

7.4.2

7.5

34004.

7.6

9378.

7.7

7.7.1

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10654;

25576 25575.

25575 25576.

8

7 .7.2

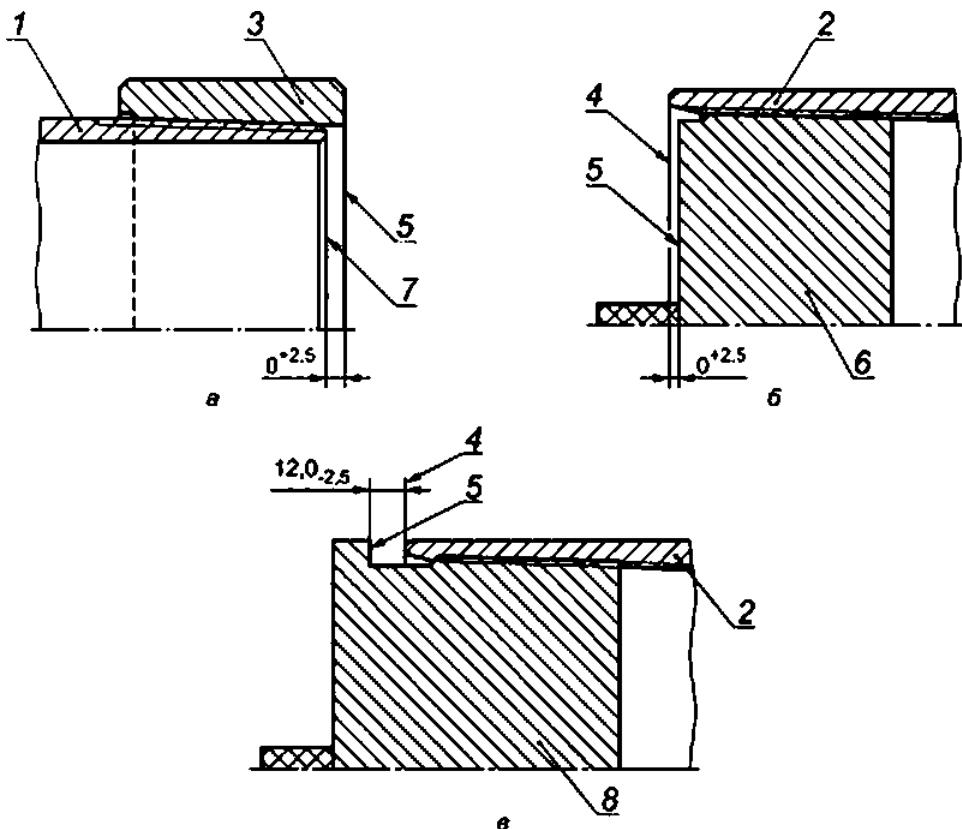
18.

*2-6

18) (

2.5).

— 0² 5 (. 18) (2.5):
 — 12.0₋₂₅ (. 18).



J— ; 2— ; 3—
— . 7— ; 4— ; —
18—

7. 7.3

19.

$24.0_{-2}^+ 5$

(. 19).

0 -

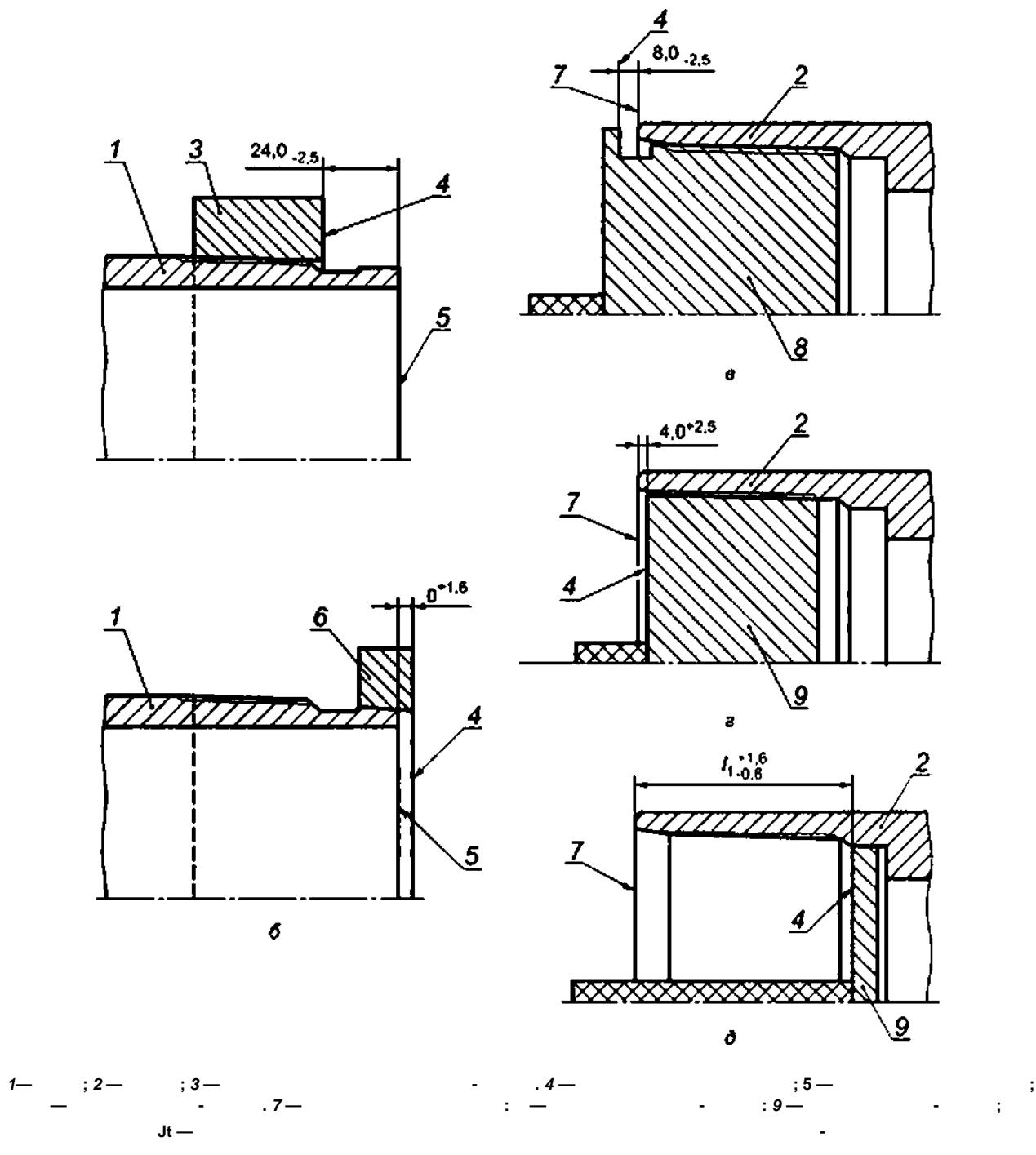
(. 19) (1.6).

:

$-8.0_{-2.5}^+$ (. 19).
 $-4.0^{+2.5}$ (. 19).

I,Q®

(. 6 19).

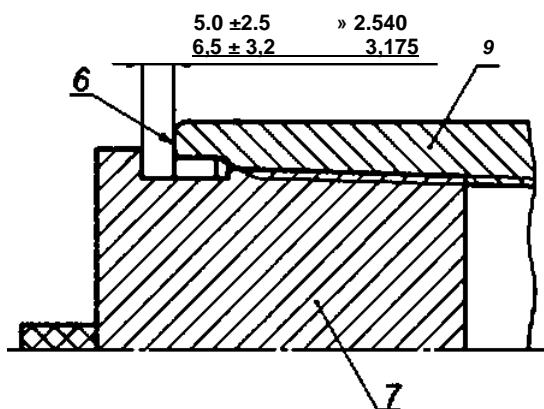


19—

7.7.4

20.

		(.)	20)	:
»(2.512.5)	—	2,540	;	
• (3.213.2)	—	3.175	.	
			(.)	20)
- (5.012.5)	—	2,540	;	
- (6.513.2)	—	3.175	.	



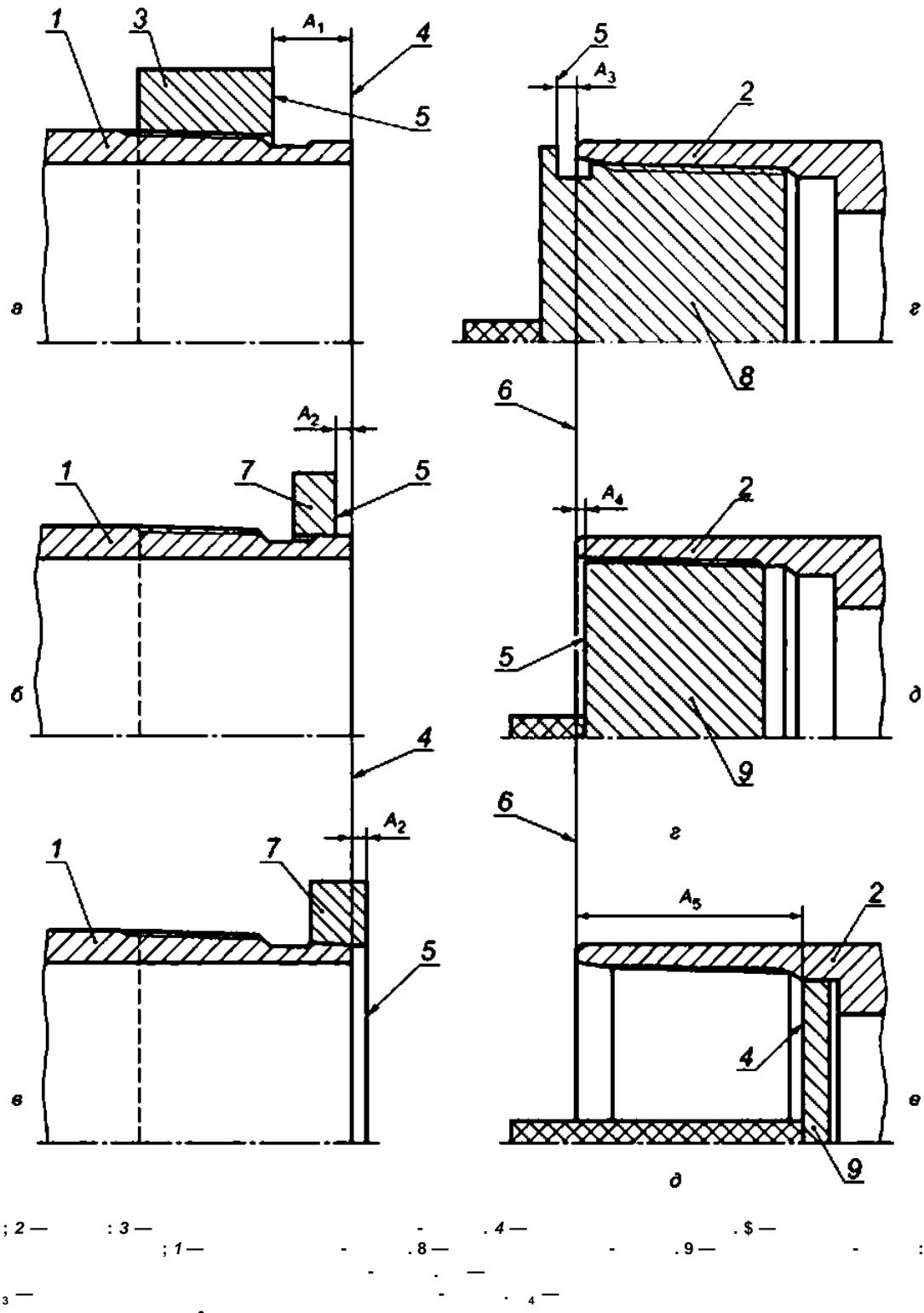
1—< , 2— ; 3— — . 4— ; 5— ; 7— ;

20—

7.7.5

21.

-) 20_{-2}^{+2} — (. 21) :
60.32 101.60 ;
-) $20.2.4$ — : 60.32 101.60 ;
-) 24_{-25}^{+2} — ? : 114.30 (. 21)
- :
): 0_{-1}^{+1} (. 21) — 60.32 101.60 (.
- 1,2);
): *1-⑧ (. 21) — 114.30 (.
1.6).
- (. 21) :
): 5.0_{-2}^{+2} — 60.32 101.60 ;
- 6) $6.0.2.5$ — 114.30 (. 21) :
4 — 60.32 101.60 (.
- 1,2);
): 6.0^{+2-5} — 114.30 (.
\$ (. 21)
- :
): 45_{-j}^{+j} — 60.32 73.02 ;
): 55_{-12}^{+12} — 88.90 101.60 ;
): 84 ijj — 114.30 .



21 —

7.9

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34057. 632 633

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